

GE Energy Consulting

NYISO IBR Roadmap Project

Presentation to New York State Reliability Council



30 November 2022

GEEnergyConsulting.com



NYISO's inverter-based resource (IBR) roadmap addresses transmission security needs for 2040



1



Technical

What risks should NYISO assess & mitigate in anticipation of 2040 IBRs?



2



Regulatory

Emerging regulatory requirements addressing IBR risks

Please note that a review of NYISO's current planning practices was not part of the scope of this IBR Roadmap. As a result, GE recommendations may overlap with existing NYISO processes and do not imply a gap in NYISO evaluations or criteria.

Anticipated 2040 reliability risks form core of NYISO IBR roadmap

Emerging regulations likely to overlap recommendations



1. WEAK GRID RISKS

- Synchronous machines (SMs) *form* today's voltage reference
- Today's IBRs *follow* the voltage reference ("grid following")
- As IBRs displace SMs, weakens voltage -> reliability risks:
Steady state and dynamic voltage stability, controls stability, angular stability risks

2. SMALL SIGNAL STABILITY RISKS

- Unwanted non-fundamental resonances due to interactions between electrical elements
- E.g. Series compensation, IBR controls, high speed exciters

3. FREQUENCY STABILITY RISKS

New risks as IBRs displace SMs:

- Frequency response obligation can't be met w/o IBRs providing response
- IBR frequency response behavior/coordination may result in unreliable outcomes

NYISO IBR ROADMAP

Top recommendations

1. Adopt new screening methods

1. Use production cost modeling to screen for new IBR risk conditions
2. Weak grid screening using SCR analysis
3. Small signal screening using frequency scan analysis

2. Develop EMT modeling capabilities

to utilize after screening methods suggest high IBR risks

3. Develop interregional evaluation approaches given high IBR levels

1. EI-wide frequency stability evaluation
2. Regional weak grid and small signal risks

Prominent IBR-related disruptions were not due to technical risks

NYISO roadmap assumes post-event NERC guidelines are followed



WHEN	WHERE	% INVERTER	DISTURBANCE	LOST GENERATION	AFFECTED TECHNOLOGIES
March 2022	Texas	60%	Severe weather	1000MW	Wind
August 2021	California	40%	Wildfires	800MW	PV, Gas, DER
July 2021	California	50%	Wildfires	800MW	PV, Gas, DER
July 2021	California	35%	Fault	550MW	PV, DER
June 2021	California	45%	Fault	1000MW	PV, DER
June 2021	Texas	30%	Failed power line	700MW	PV
May 2021	Texas	45%	Failed electrical equipment	1300MW	Gas, PV
July 2020	California	50%	Failed power line	1200MW	PV
May 2019	California		Birds nest on power line	1000MW	PV, DER
April 2018	California	30%	Failed power line	1200MW	PV, Gas, DER
Oct 2017	California		Wildfires	1600MW	PV
Sept 2016	S. Australia	50%	Lightning	State-blackout	Wind, Coal, Gas

Events could have been avoided if pre-existing NERC guidelines were followed

- **IBRs w/ outdated unreliable performance attributes**
NERC 2019 reliability guideline outlines required performance attributes (e.g. momentary cessation, phase jump immunity) that weren't followed
- **Poor IBR modeling practices**
NERC 2019 reliability guideline outlines modeling improvements such as use of EMT models & validation that weren't followed

<https://www.nerc.com/pa/rrm/ea/Pages/Major-Event-Reports.aspx>
https://www.nerc.com/pa/Documents/IBR_Quick%20Reference%20Guide.pdf
<https://www.aer.gov.au/wholesale-markets/compliance-reporting/investigation-report-into-south-australias-2016-state-wide-blackout>
https://www.nerc.com/comm/RSTC_Reliability_Guidelines/Reliability_Guideline_IBR_Interconnection_Requirements_Improvements.pdf



Weak grid risks

The displacement of grid-forming synchronous machines with grid-following IBRs weakens grid reference



Weakening voltage reference increases four related risks

1

Steady state
voltage stability

Voltage can collapse in weak grids w/ higher power injection + high IBRs

2

Dynamic voltage
stability

Voltage can collapse in weak grids after a disturbance

3

Controls
stability

IBRs have multiple control layers/modes ... weak grid -> control confusion

4

Angular
stability

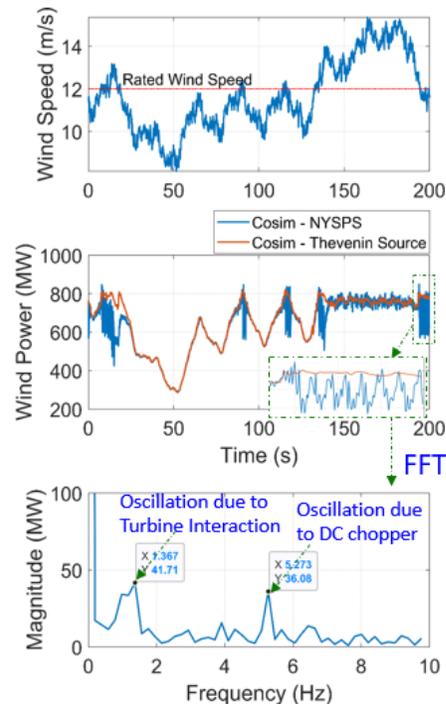
Weak grids increase risk of SMs losing synchronism after faults



Turbine-to-turbine interactions

Control Interaction in Empire Wind 1

- Two cases are conducted to verify the performance:
 - Case 1: Empire Wind 1 connects to Thevenin equivalent source in RTDS. Short-circuit power is calculated by peak fault current at Gowanus bus.
 - Case 2: Empire Wind 1 connects to full NYSPS model in RTDS.
- Two cases are tested under condition of dynamic wind speed.
- Case 1 (Cosim - Thevenin Source) is working normally.
- Case 2 (Cosim - NYSPS): transition between regions 2 and 3 causes significant oscillation at frequencies of 1.4 and 5.3 Hz
 - Traditional local controls stability assessment procedure may not be sufficient
 - Controls instability risks due to interactions among:
 - Detailed farms and NYS system
 - Wind turbines



CLARKSON + NYPA AGILE LAB CONTROLS STABILITY MODEL

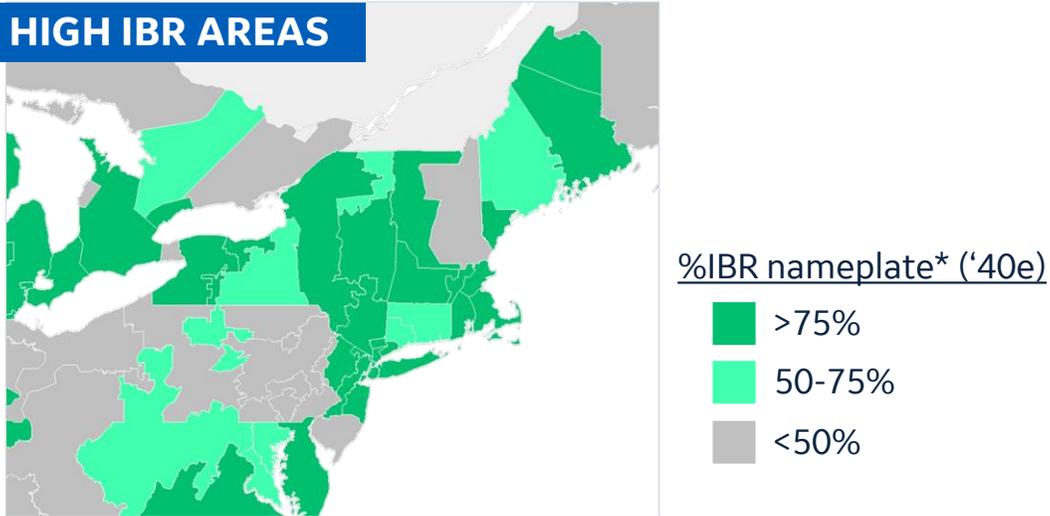
- 9GW offshore wind via Opal-RT simulator
- Onshore NY system via RTDS based on NYISO 2018 PSSE & Aspen models

Possible **weak grid** risk conditions in 2040 New York?

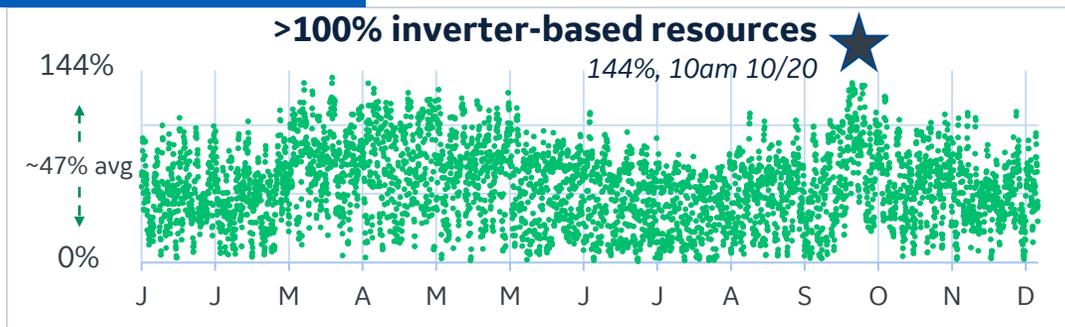
High risk scenarios conditions to study



HIGH IBR AREAS



HIGH IBR HOURS



* % IBR = Nameplate IBR / (IBR + Hydro + Nuc + Gas & Coal) ... >20MW units, SMs>75% online

Ref: GE Energy Consulting's non-proprietary forecast, ABB Hitachi

1 - <https://www.nerc.com/pa/Stand/Reliability%20Standards%20Complete%20Set/RSCCompleteSet.pdf>

NY ISO IBR ROADMAP PROJECT

High risk geographic/operating conditions

1. **High IBR penetration**/low synchronous commitment ... likely *regionally* weak grid condition
2. **High IBRs/multiple IBRs on same AC bus:** Likely a *locally* weak grid
3. **HVDC connections** (e.g. offshore wind)
4. **Neighboring jurisdictions w/high IBRs**

Regulatory note:

Generally silent on geographic guidance:

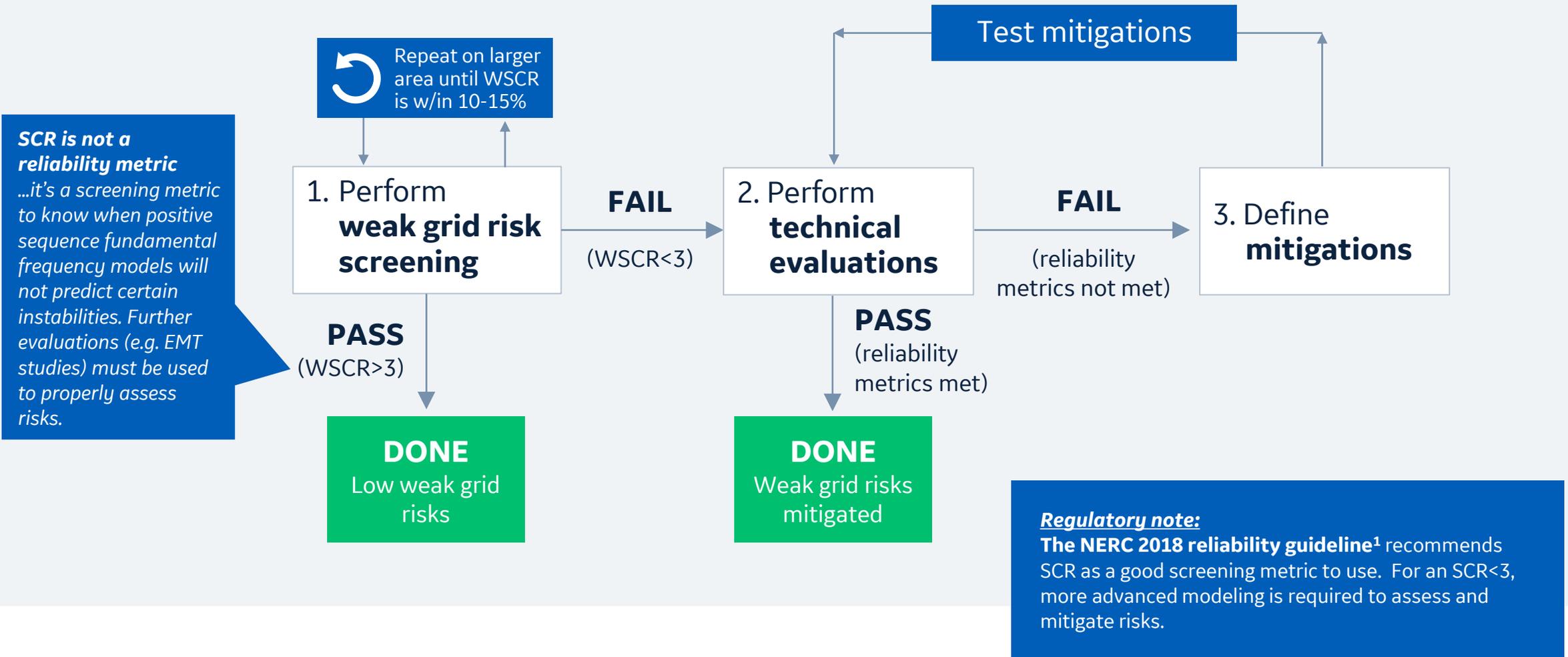
1. **NERC** guidance is generally silent on how to define the geographic coverage for weak grid screening & assessment.
2. **FERC's** upcoming interregional NOPR recognizes need for coordinated interregional planning but has yet to provide guidance regarding the need for coordinated weak grid screening. NOPR comments are highlighting the need for more.

Operating conditions:

1. **NERC:** NERC TPL-001¹ specifies peak load, off-peak but not other conditions. SAR has been opened & industry experts may weigh in.
2. **FERC:** Standards not covering system conditions ... yet. Comments to the FERC Interconnection NOPR are highlighting need for more guidance here.

Recommended weak grid planning approach

WSCR used as a screening metric for further EMT evaluations



1 - https://www.nerc.com/comm/RSTC_Reliability_Guidelines/Inverter-Based_Resource_Performance_Guideline.pdf
N ISO IBR ROADMAP PROJECT

Weak grid risks technical evaluation approach



RISKS	STUDIES				METRICS		MITIGATION	
	CONDITIONS	SCREEN	LF	DYN	EMT	COMPLIANCE METRICS		GE RECOMMENDED METRICS
WEAK GRID RISK		WSCR					WSCR >3	Additional studies below
Steady state voltage stability	<ul style="list-style-type: none"> High IBRs same AC line Multiple IBRs same AC line HVDC connection High IBR neighbors N-X w/ high IBR Faults, trips 		✓			Normal: $-5% < V_{rating} < +5%$	$\Delta V / \Delta P > 0.95$ p.u.	<ul style="list-style-type: none"> IBR tuning Synchronous condensers Interregional transmission Future: Grid forming IBRs
Dynamic voltage stability				✓	✓	<ol style="list-style-type: none"> Normal: $-5% < V_{rating} < +5%$ Fault ride through: No trip within voltage envelope 	No voltage collapse post-fault/trip	
Controls stability				✓	✓	Avoid unwanted interactions	Enter/exit control modes “cleanly” <ul style="list-style-type: none"> No observed hysteresis on limits During/post VRT behavior well mannered 	
Transient stability				✓	✓	PRC 024: Exemption you must not trip unless you are going to damage unit	<ol style="list-style-type: none"> Angle: 1st swing system angle “clean” recovery Trips: Ok if limited system impact Voltage swing: post-clearing voltage dips moderate 	

Regulatory note:

NERC SARs will likely require EMT studies¹

- TPL-001:** EMT studies must be performed for planning
- FAC-002:** EMT studies must be performed for interconnection

1 - <https://www.nerc.com/pa/Stand/Pages/Project2022-04EMTModeling.aspx>

Weak grid risk technical evaluation **model recommendations**



LOAD FLOW MODELS:

1. **Plant-level IBR voltage control models** including real and reactive power flow models. Inverter-level behavior will be captured in EMT models.
2. **Aggregated representation of each IBR plant** using one equivalent machine model is sufficient

DYNAMICS MODELS (i.e. positive sequence):

1. **Aggregated IBR plant models sufficient** for planning and interconnection studies
2. **Protection dynamics models** to be included
3. **Model acceptance criteria to allow user-written models** with sufficient detail
 - Functional-level representation of all control loops at inverter & plant. Generic models typically do not allow full representation.
 - Acceptable model validation criteria for model to match field equipment performance.
 - Generator & plant protection ... and limiters need to be included.
 - New technologies (e.g. grid forming) should be represented. Such technologies rarely represented sufficiently in generic models.

EMT/TRANSIENTS MODELS

1. **Similar recommendations as dynamics**
2. **Developer EMT models** should be required
3. **Benchmarking between EMT & dynamics** models

Regulatory note:

1) *Use of transients/EMT models will likely be required:*

- **IEEE 2800 & 2800.2¹:** Recommends EMT models used to assess IBR risks. Protection models should be included.
- **NERC MOD-032 (SAR)²:** EMT models must be used in planning

2) *Acceptance criteria for user-written models:* NERC MOD 26³ update to require planners to develop model acceptance criteria for dynamics and EMT user-written models.

3) *Benchmarking:* MOD 26 (SAR) calls out need for benchmarking between dynamics and EMT models

1- <https://standards.ieee.org/ieee/2800/10453/>

2 - <https://www.nerc.com/pa/Stand/Pages/Project2022-04EMTModeling.aspx>

3 - https://www.nerc.com/pa/Stand/Pages/Project-2020_06-Verifications-of-Models-and-Data-for-Generators.aspx

Weak grid **risk mitigation recommendations**



BASELINE REQUIREMENTS

1. **Adopt IEEE 2800 requirements** to establish minimum capability to support grid stability.
2. **Require/incentivize IBR voltage regulation even with no wind or sun ...** especially important during light load
3. **Follow NERC IBR event report recommendations¹ ...** A prerequisite to this roadmap.

SYNCHRONOUS CONDENSERS:

1. **Retrofitting existing gas or oil generation**
2. **Building new condensers** (e.g. LIPA recommended \$200M of new condensers to interconnect 3GW offshore²)

IBR SOLUTIONS:

1. **Control tuning:** A number of pre-configured settings available suit varying grid conditions including weak grid (e.g. voltage regulator gains, current limits, ride through settings, etc.)
2. *(Future)* **Grid-forming controls:** Not commercial today on all IBR technologies but a piloting opportunity. Lower space requirement, cost and offshore deployment vs condensers.

INTERREGIONAL REINFORCEMENT

- **Connecting to stronger grids** can improve xSCR
- **DC connections** should be considered if connecting to weaker grids (e.g. offshore network).

Ref:

1 - https://www.nerc.com/pa/Documents/IBR_Quick%20Reference%20Guide.pdf

2 - <https://www.lipower.org/wp-content/uploads/2021/02/13.-Briefing-on-Grid-Planning-Climate-Ladership-Community-Protection-Act.pdf>



— Small signal stability risks

High risk **small signal stability** conditions in 2040 New York?



High risk scenarios conditions to study

E.g. Proposed T019 345kV path includes 50% series compensation

Town	Proposed Work	Miles	Change in No. of Structures
Schodack	New Knickerbocker 345kV Switching Station on utility-owned land	-	-
Schodack		2.6	+4
Stuyvesant		8.0	-4
Stockport		4.5	+3
Ghent	Holds a new 345kV line and one existing 115kV line	0.8	No Change
Claverack		6.3	+12
Claverack	Rebuild the existing Churchtown 115kV Switching Station on existing utility-owned land	-	-
Livingston		2.2	No Change
Claverack		1.0	-7
Livingston		8.3	-60
Gallatin		1.2	-9
Clermont		0.7	-4
Milan		8.0	-76
Clinton		8.0	-59
Pleasant Valley	Holds a new 345kV line and one existing 115kV line	5.1	-38
Pleasant Valley	New Van Wagner Capacitor Bank Station and upgrades to Pleasant Valley Substation	0.8	+5

*All mileage and structure change information is approximate.

Commitment/dispatch/location conditions

- IBRs near series compensation:** Can result in subsynchronous resonance (SSR) which can trigger subsynchronous controls interaction (SSCI) or subsynchronous torsional interaction (SSTI)
- IBRs w/high AC cable charging** (e.g. large Offshore plants w/AC cabling)
- Weak grid conditions:** Represents a low damping condition which can result in sustained oscillations
- SMs w/ high speed exciters:** Not specifically related to IBRs ... NYISO may have processes in place if they have such SMs
- Torsional interaction conditions:** If there are series capacitors in NYISO & the power flows only through that path from IBR pockets or a single SM, then there is likely to be SSR or SSCI & a more comprehensive analysis needs to be commissioned by experts in torsional interaction.
- N-X grid conditions:** While the N-0 grid may be strong enough to damp out oscillations, the N-X grid may not be strong enough

Clarkson & NYPA observing small signal stability risks w/NY offshore

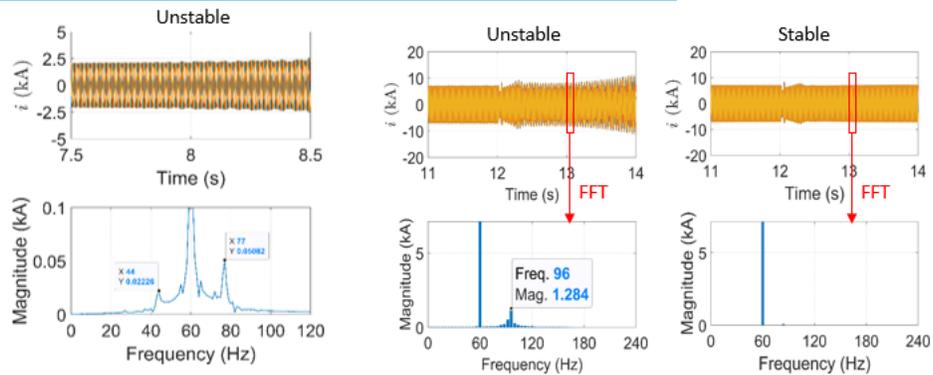
EMT modeling enables risk assessment & mitigation of non-fundamental frequency oscillations



SUSTAINED PLANT-TO-PLANT OSCILLATIONS ACROSS EMPIRE 1 AND EMPIRE 2

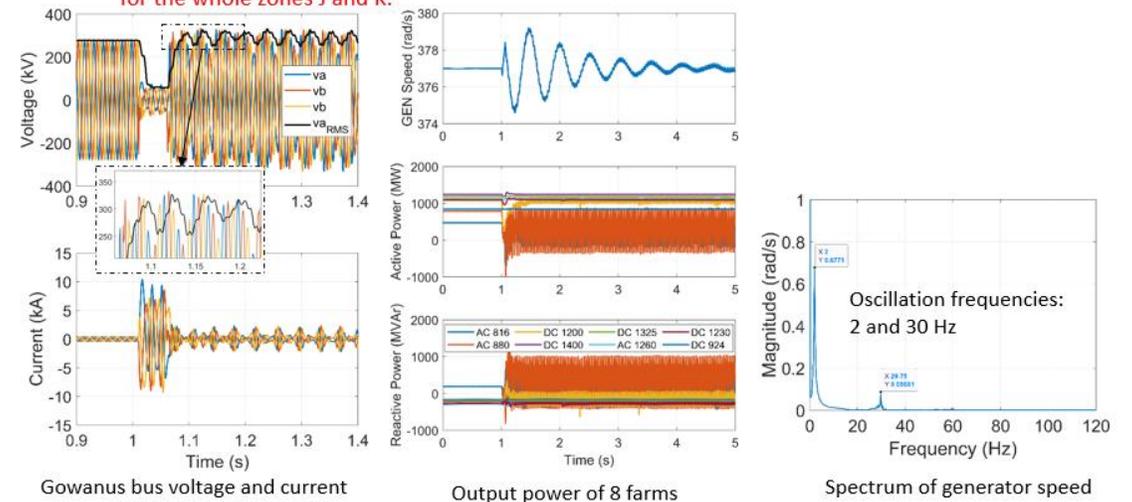
FRT Performance of Empire Wind 2 – 1260 MW behind Equivalent source (Local)

- Wind farm operates at the rated power.
- High impedance fault at offshore collector bus is applied at 12s and it is clear after 8 cycles.
- Voltage and current are measured at POI
- FFT analysis of POI current shows the resonance frequency of 44, 77, and 96 Hz in the unstable cases
- **Harmonic and subsynchronous instabilities**
- Optimal tuning the controller gains mitigates the resonance.



SUSTAINED OSCILLATIONS ACROSS 9GW OFFSHORE FLEET

- Three-phase-to-ground fault at GOETHLS bus; fault impedance is 0.1Ω and fault duration is 3 cycles.
- Significant oscillation in three farms: AC816, AC880, and DC1200.
- Sustained voltage oscillation at 30Hz at Gowanus
- Sustained frequency oscillation at 2Hz and 30Hz
- The grid is weaker due to 9GW pumped to Zones J and K. The Short Circuit Power is being evaluated for the whole zones J and K.



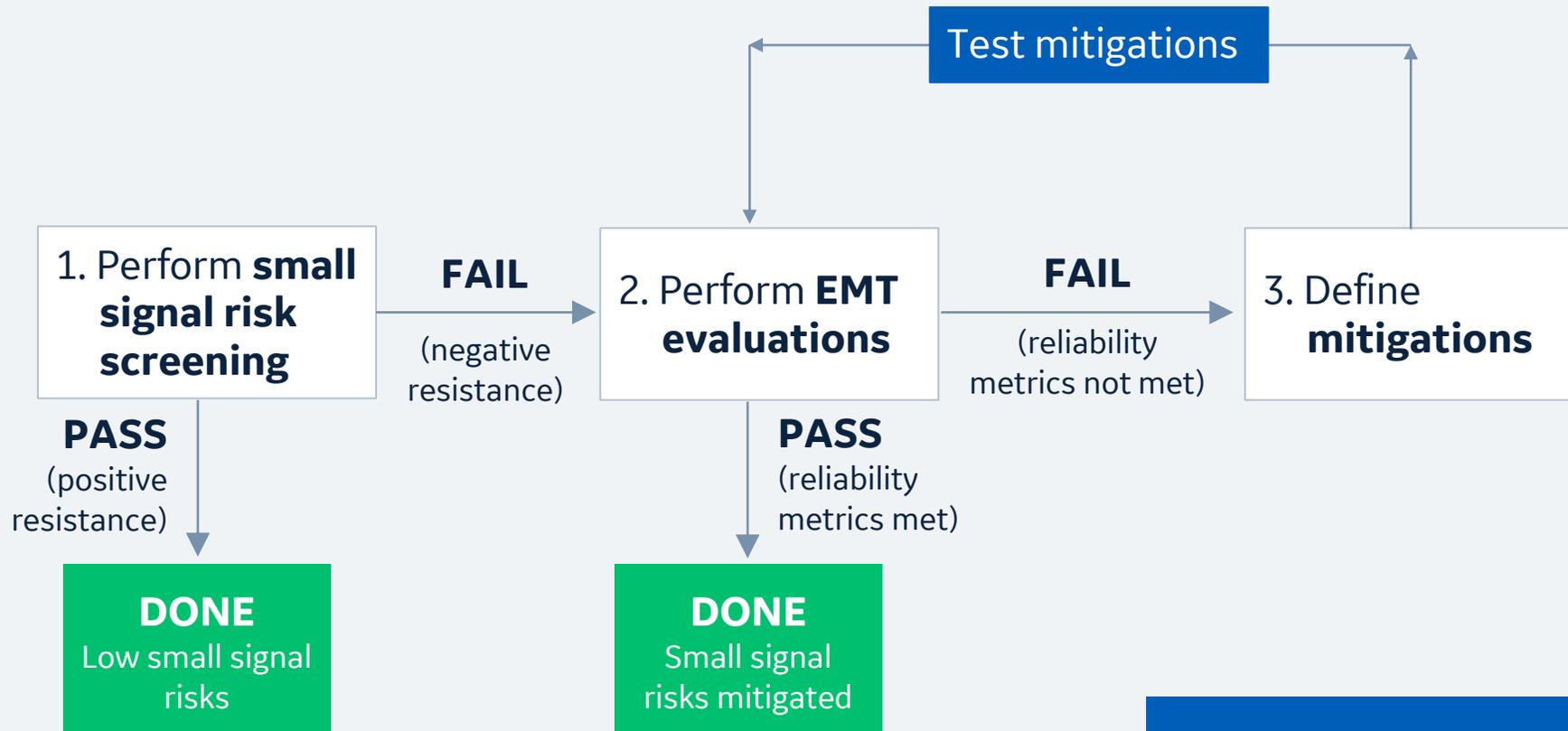
Gowanus bus voltage and current from GEOTHS to GOWANUS

Output power of 8 farms

Spectrum of generator speed



Recommended small signal stability planning approach



Regulatory note:

Small signal stability is currently not addressed by industry standards or regulations.

Small signal stability risks technical evaluation approach



RISKS	STUDIES				METRICS		MITIGATION	
	CONDITIONS	SCREEN	LF	DYN	EMT	COMPLIANCE METRICS		GE RECOMMENDED METRICS
SMALL SIGNAL STABILITY	<ul style="list-style-type: none"> High IBRs same AC line Multiple IBRs same AC line HVDC connection High IBR neighbors N-X w/high IBR Torsional condition Faults, trips 	Freq scan					Negative resistance	Additional studies below
SSR					✓		Damping factor (ζ) $\gg 0.1$ (Critically damped) Phase angle (δ) $< 90^\circ$	<u>S</u> M:s: torsional stress relays (TSRs) <u>I</u> BRs: IBR settings tuning, grid strengthening
Power swings				✓	✓			<u>S</u> M:s: Power system stabilizers (PSS)
Super-synchronous oscillations					✓			<ul style="list-style-type: none"> Tuning IBR gains Passive filters

Model recommendations:

- 1. IBR models:** specific EMT models that capture SSCI risk (e.g. low frequency behavior captured)
- 2. Protection models** as it relates to SSCI risk (e.g. low frequency behavior)
- 3. Interregional** given potential interregional interactions (e.g. if series comp in PJM on AC line to NY)

Small signal stability **risk mitigation recommendations**

Mitigations depend on the type of resonance



SSR MITIGATIONS

- 1. Low Level of Series Compensation** to avoid SSR
- 2. Topology/Power-Based Switching Schemes**
- 3. Tuned IBR controls** to add damping and mitigate SSCI.
- 4. Supplementary Excitation Damping Control (SEDC)**
5. Properly tuned **thyristor-controlled series capacitors**
- 6. SVC-type SSR Damper**
- 7. Passive SSR Bypass Filter** on series capacitor bank
- 8. SSR Blocking Filters**

LOCAL AND INTER-AREA OSCILLATIONS

- 1. Power system stabilizers (PSS):** Generally, an active filter on an SM ... similar capability can be deployed with an SEDC
- 2. Generation curtailment:** Avoid oscillations through reduced power flow

SUPER-SYNCHRONOUS OSCILLATIONS:

- 1. Control tuning:** to increase damping
- 2. Passive filters:** more expensive vs IBR tuning

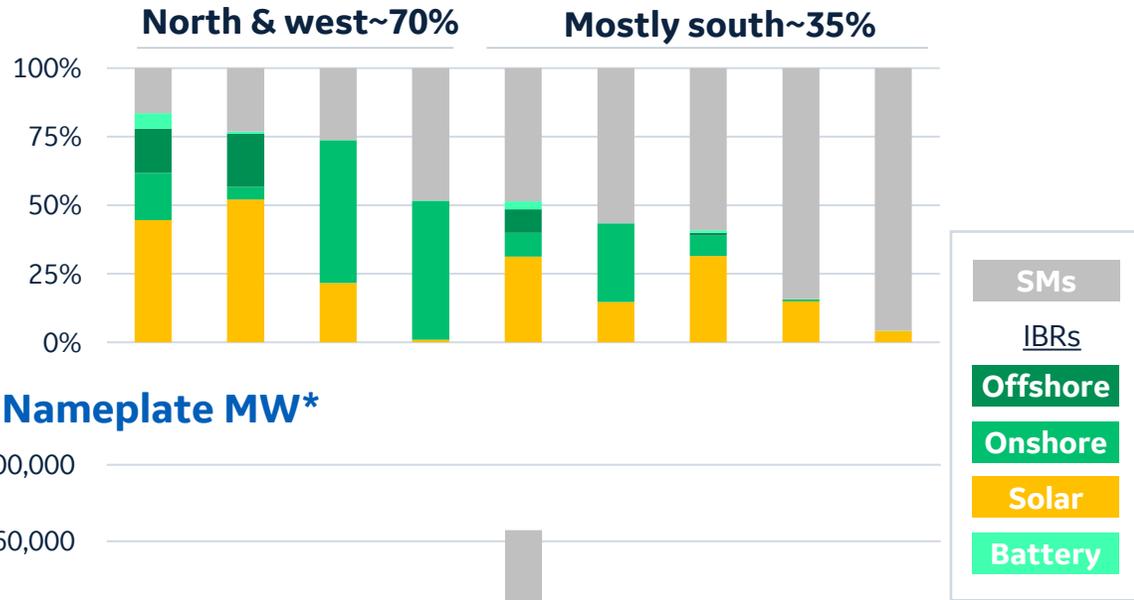


— Frequency stability risks

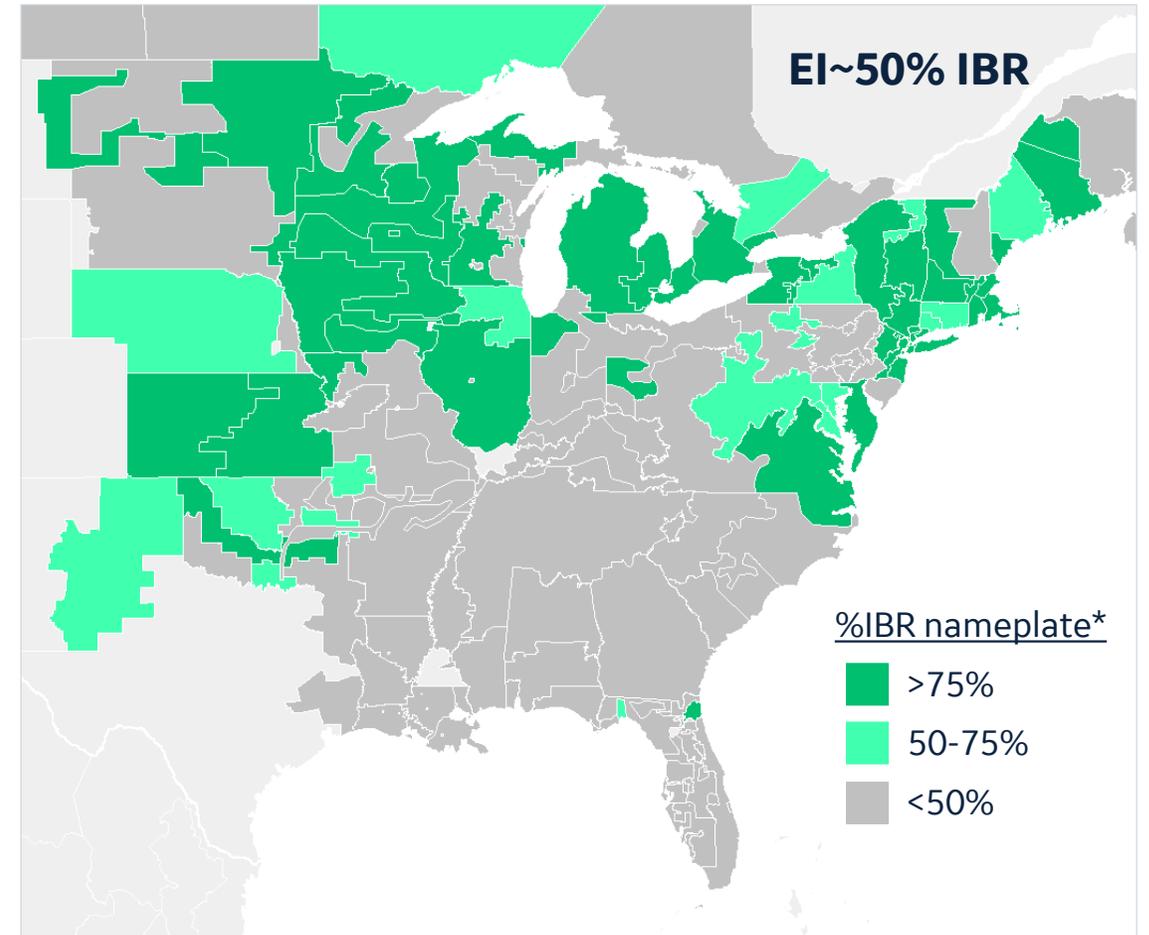
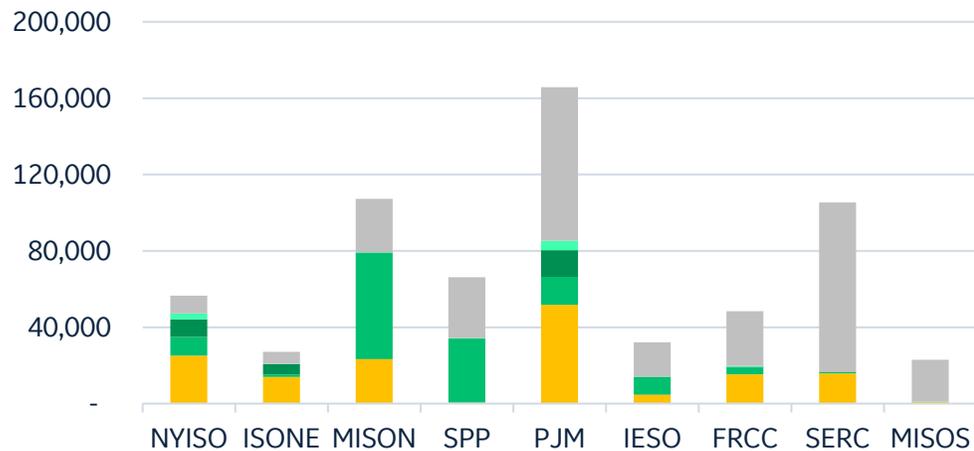
By 2040, the Northeast & Western parts of the Eastern Interconnect will depend on IBRs ... is frequency stability at risk?



%IBR nameplate*

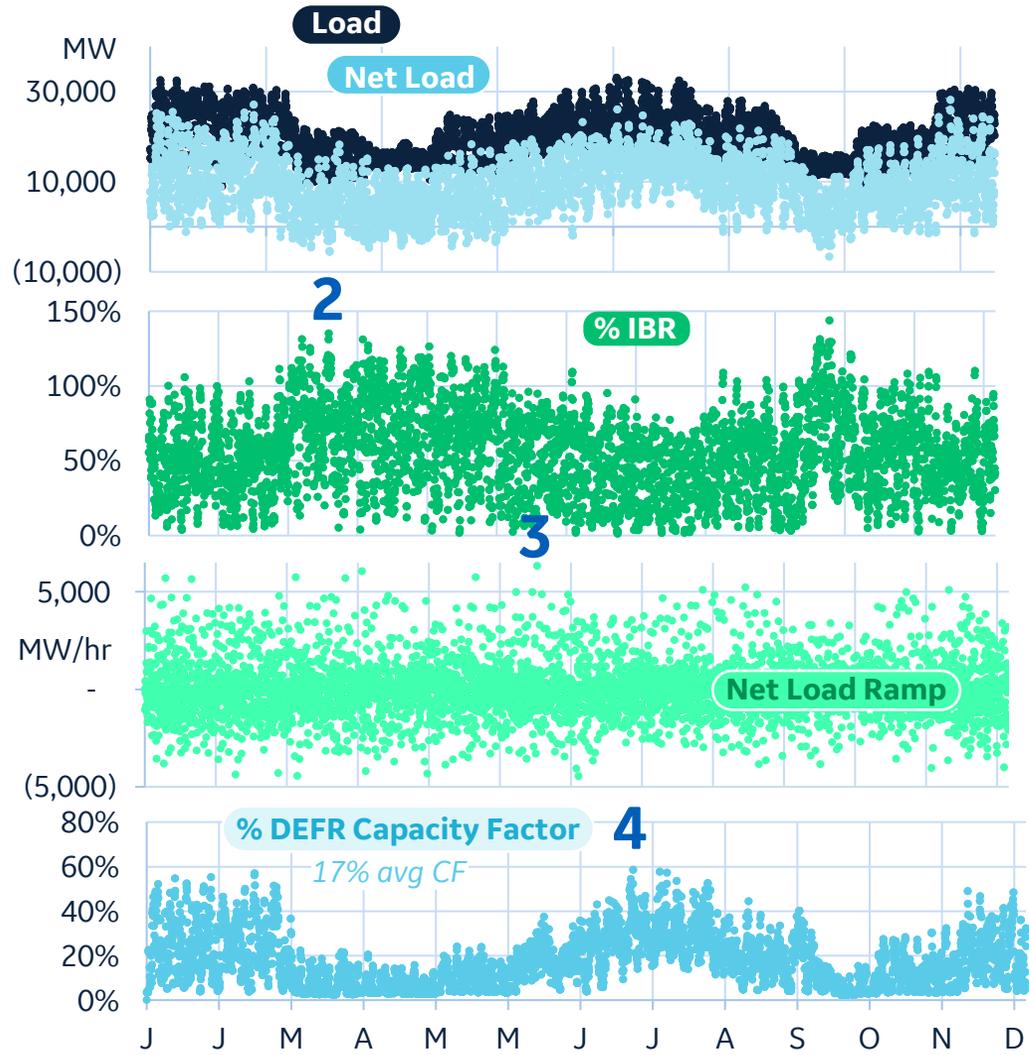


Nameplate MW*



* % IBR = Nameplate IBR / (IBR + Hydro + Nuc + Gas + Coal) ... units >20MW & SMs >75% online

High risk frequency stability conditions in 2040 New York?



Commitment/dispatch conditions

1. **Coordination across EI:** How to *reliably* meet NY's (likely higher) FRO w/IBRs?
2. **Low inertia:** High IBR/low synchronous commitment
3. **High ramping:** Can the remaining units ramp quickly enough? Is there enough headroom left in system?
4. **Low synchronous headroom:** Not enough ability to support underfrequency
5. **N-X conditions:** That may result in high IBR/low inertia

Regulatory note:

Interregional coordination:

1. **NERC** BAL-003-1.1 (SAR)¹ how to update IFRO but open question about IBR performance requirements
2. **FERC's** upcoming Interregional NOPR recognizes need for coordinated interregional planning but hasn't addressed frequency stability

Operating conditions:

1. **NERC:** NERC TPL-001² specifies peak load, off-peak but not other conditions. SAR has been opened & industry experts may weigh in.
2. **FERC:** Standards not covering system conditions ... yet. Comments to the FERC Interconnection NOPR are highlighting need for more guidance here.

Ref: GE Energy Consulting, non-proprietary database

1 - <https://www.nerc.com/pa/Stand/Pages/Project201701ModificationstoBAL00311.aspx>

2 - <https://www.nerc.com/pa/Stand/Reliability%20Standards%20Complete%20Set/RSCCompleteSet.pdf>

NY ISO IBR ROADMAP PROJECT

Frequency stability risk technical evaluation approach



RISKS	STUDIES					METRICS		MITIGATION
	CONDITIONS	SCREEN	LF	DYN	EMT	COMPLIANCE METRICS	GE RECOMMENDED METRICS	
FREQUENCY STABILITY	<ul style="list-style-type: none"> • 2040 EI-wide • Low inertia • High net load ramping • Low SM headroom • N-X resulting in low inertia 		✓	✓		1. FR > NY FRO in 2040 2. MDF < 420 mHz 3. Nadir > 59.5Hz	1. Recovery well mannered > critical damped 2. Settling time < 15sec	<ul style="list-style-type: none"> • New IBRs provide: FFR, PFR, FRT, Reg • Tune IBR response • Tune SM performance • New operating/resource limits • Network reinforcements

Model recommendations:

- 1. EI-wide models** to assess reliable IBR FR participation.
- 2. IBR frequency response control models** for dynamics simulations
 - a) Fast frequency response (FFR)** control models. User-written or updated 3rd generation generic models should be used to evaluate FFR.
 - b) Primary frequency response (PFR)** control models
- 3. Non-IBR protection models** to assess unwanted tripping during grid frequency events

Frequency stability risk mitigation recommendations



IBR CONTROLS

1. Require new IBRs to provide:
 - a) **Fast frequency response** (FFR)
 - b) **Primary frequency response** (PFR)
 - c) **Fault ride-through** capability

2. Tune frequency response settings

OPERATING/RESOURCE LIMITS

1. Real time **inertia monitoring** + operating protocols to remain above floor
2. **Geographic limits** for FR participation (e.g. by zone)
3. **Technology limits** for FR participation (e.g. SMs vs IBRs)

NETWORK UPGRADES

Flywheel addition to synchronous condensers

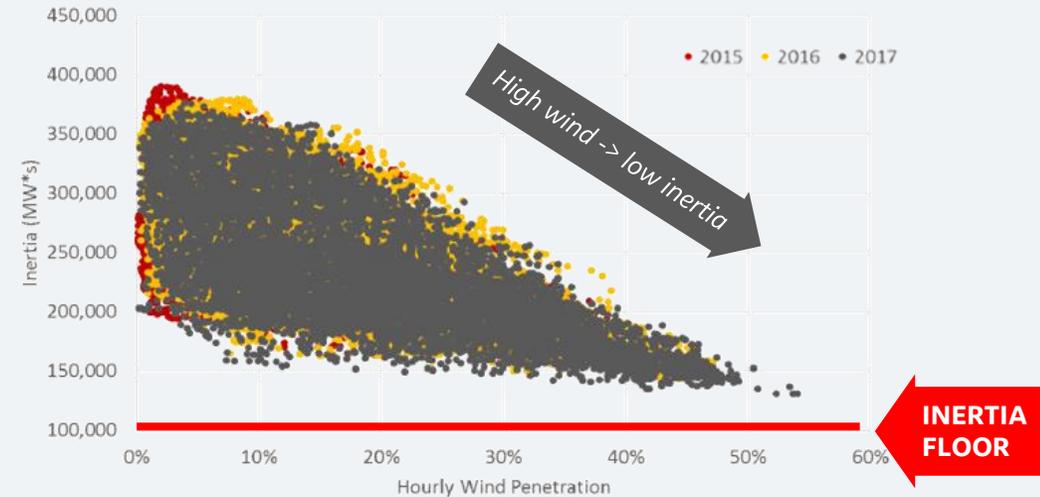
Regulatory note:

- IEEE 2800¹: Minimum PFR & FFR performance standards
- NERC & FERC, most Balancing Authorities: yet to adopt minimum performance standards for IBR frequency response. Texas, New England & MISO assessing piecemeal adoption of 2800.
- FERC 842²: Requires IBR capability to provide FR, but does not define how to implement in practice to meet FRO and reliability needs.

1- <https://standards.ieee.org/ieee/2800/10453/>
 2- <https://www.ferc.gov/sites/default/files/2020-06/Order-842.pdf>

EXAMPLE: ERCOT TRACKS REAL TIME INERTIA

Synchronous inertia vs. hourly wind penetration



Emergency BPs	Inactive	Emergency BPs	Inactive	Emergency BPs	Inactive
System Inertia	119,999 MW-s	System Inertia	109,999 MW-s	System Inertia	99,999 MW-s
SCED	00:03:08	SCED	00:03:24	SCED	00:04:00
RLC	00:00:06	RLC	00:00:06	RLC	00:00:06
STLF Forecast High	21.6	STLF Forecast High	21.6	STLF Forecast High	21.6
STLF Next 30 Mins	Normal	STLF Next 30 Mins	Normal	STLF Next 30 Mins	Normal
QSE ICCP	Normal	QSE ICCP	Normal	QSE ICCP	Normal

OPERATOR DISPLAY: REAL TIME INERTIA

Source: *Inertia: Basic concepts & impact on the ERCOT Grid*, courtesy Julia Matevosyan, 2018

NYISO IBR roadmap: anticipated 2040 reliability risks inform next steps



1. WEAK GRID RISKS

As IBRs displace SMs, weakens voltage -> new reliability risks:
Steady state and dynamic voltage stability, controls stability, angular stability risks

2. SMALL SIGNAL STABILITY RISKS

Unwanted non-fundamental resonances due to interactions between electrical elements
E.g. Series compensation, IBR controls, high speed exciters

3. FREQUENCY STABILITY RISKS

New risks as IBRs displace SMs:

- Frequency response obligation can't be met w/o IBRs providing response
- IBR frequency response behavior/coordination may result in unreliable outcomes

NYISO IBR ROADMAP

Top recommendations

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2. Weak grid screening using SCR analysis
3. Small signal screening using frequency scan analysis

2. Develop EMT modeling capabilities

to utilize after screening methods suggest high IBR risks

3. Develop interregional evaluation approaches given high IBR levels

1. EI-wide frequency stability evaluation
2. Regional weak grid & small signal risks



ERCOT



Generator Interconnection Study Queue (OCT'22)

Fuel type	IA signed & FIS done or underway	Total in Queue (SS complete)
CCCT + CT Gas	6,269 MW	9,606 MW
Wind	16,726 MW	23,025 MW
Solar	98,898 MW	122,585 MW
Battery	59,357 MW	75,630 MW

<http://www.ercot.com/gridinfo/resource>

- New RRS A/S co-optimized with Energy
- Must meet min. performance specified in NP
- Procure min amount to sustain nadir > UFLS

Prior Framework

Regulation
157 to 687 MW*

Responsive Reserve Service

1. PFR
2. Load Resources on Under Frequency Relay (UFR)
3. 10 minute ramp

2,300 to 3,200 MW*

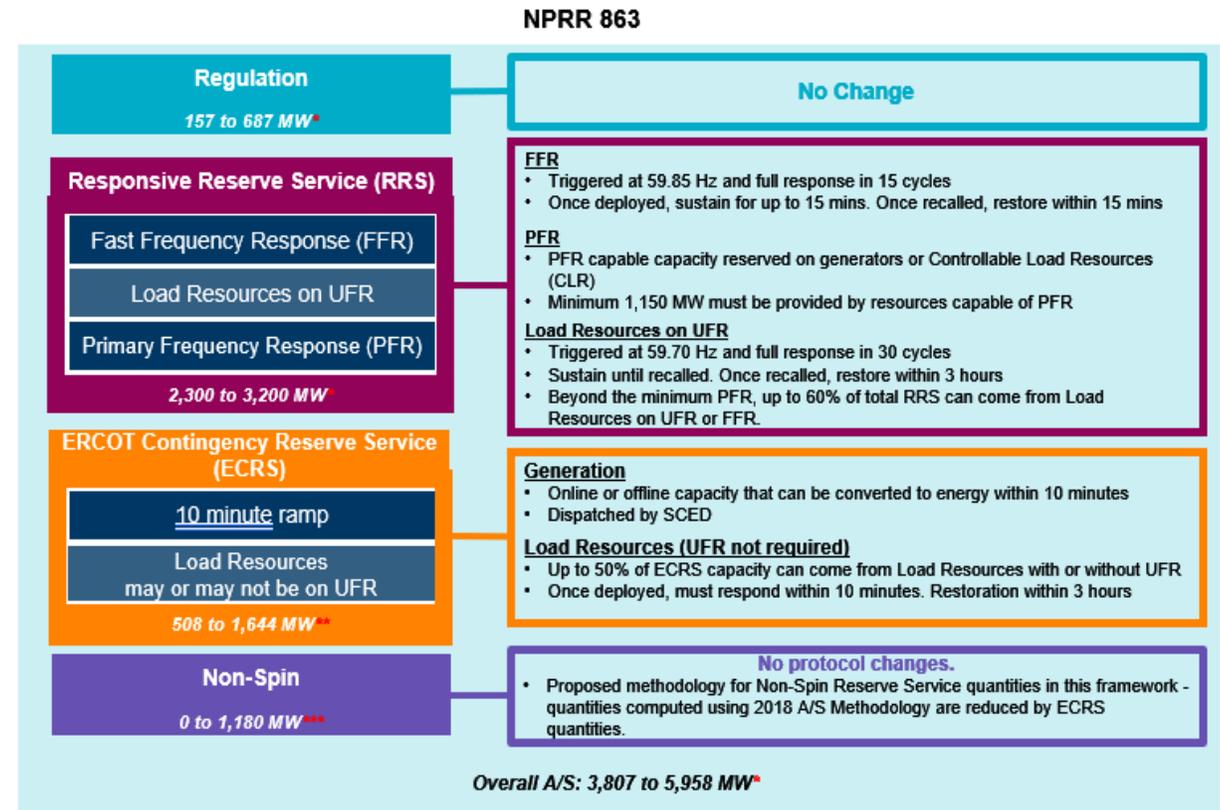
Non-Spin
967 to 2,361 MW*

Overall A/S: 3,807 to 5,958 MW*

New Ancillary Service Products - NRR 863:

New Responsive Reserve included as of March 2020

RRS is a market-based approach for procuring frequency services.



*Quantities computed/estimated using 2018 Ancillary Service Methodology. **Quantities estimated using this reference. ***Quantities estimated using this reference and method in box on far left. For Discussion Purposes Only. The intent of this slide is to represent NRR 863 (with STEC comments from 10/1/2018). Protocol language prevails to the extent of any inconsistency with this one page summary.

PUBLIC

New York is aiming for +40GW IBRs by 2040

Significantly higher in-state generation may increase frequency response obligation



Requirements

- 70% RE x 30
- 6GW PV x 25
- 3GW storage x 30
- 9GW offshore x 35

Assumptions

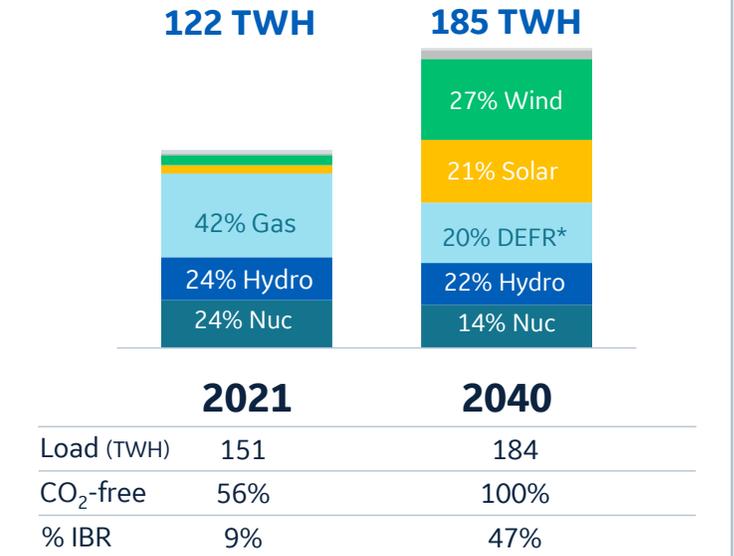
- Load: NYISO baseline view
- Gas: Converts to “Dispatchable Emission-Free Resource” (DEFR) by ‘40
- Imports/Exports: flexible
- REN: NYISO 70x30 scenario
- Electrification: NYISO ... picks up post ‘40

Nameplate (GW)

Type	'21 (GW)	'40 (GW)	Δ
Gas	23	23	-
Hydro	5	5	-
Nuclear	4	3	-1
Solar	5	26	+21
Onshore	3	10	+7
Offshore	0	9	+9
Storage	2	5	+3
Other (Oil)	4	4	-
Total	47	84	+37

**+40GW
IBR**

In-state generation (TWH)

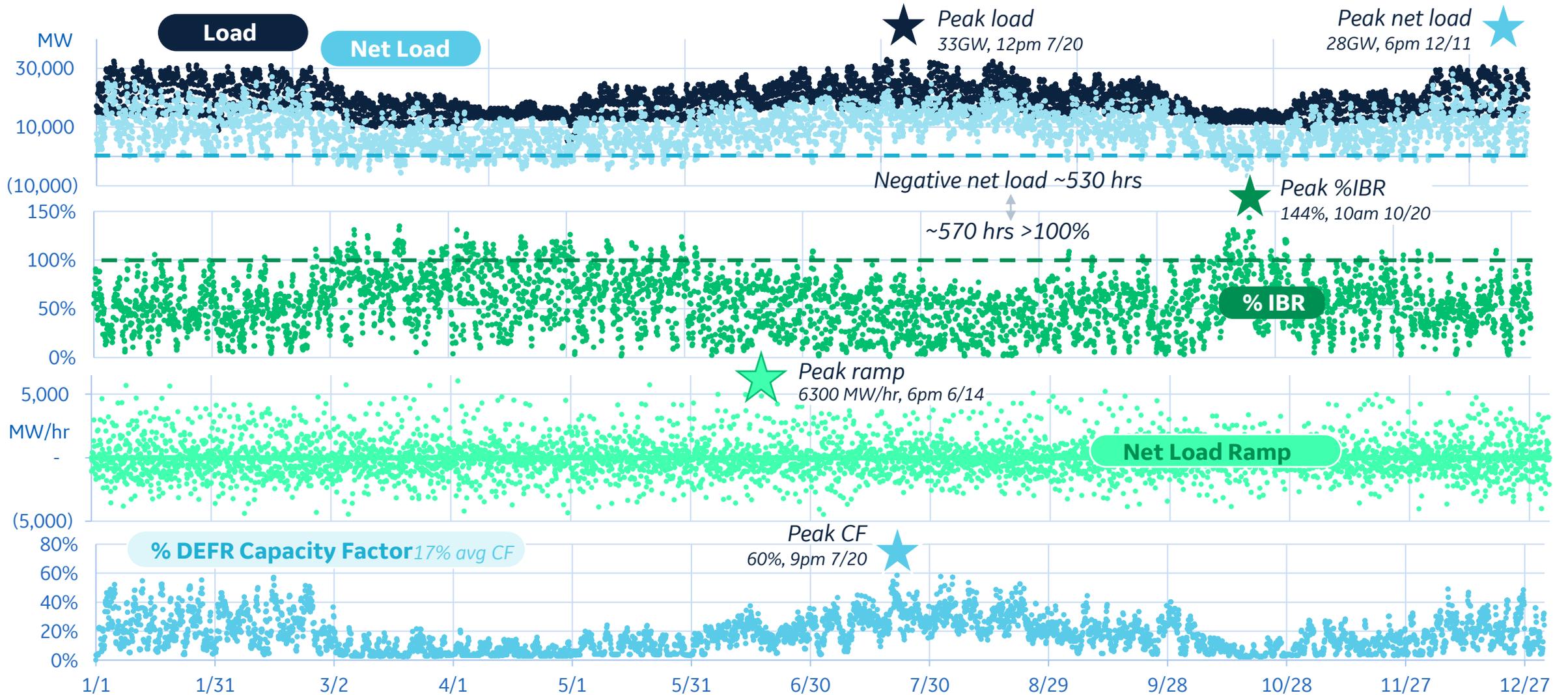


*DEFR = Dispatchable Emission-Free Resource

New York 2040: New off-peak conditions to plan around



NYISO production cost modeling can help identify new hours of IBR risk

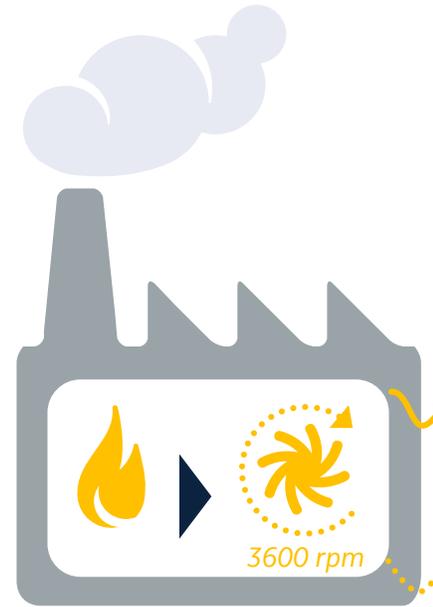


NYISO roadmap challenge: IBRs form voltage and frequency differently from synchronous machines



MECHANICAL:
voltage & frequency
are created by
mechanical rotation

- 1. CREATES VOLTAGE** reference
- 2. SLOW:** Changes in ~seconds
- 3. FIXED:** Less configurable



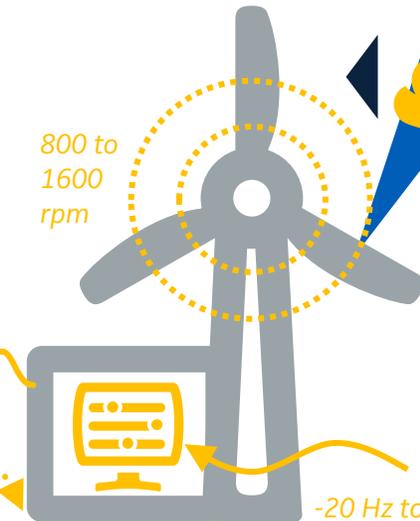
SYNCHRONOUS MACHINES (SMs)
Gas, nuclear, hydro, coal

OUTPUT

230kV, 60Hz AC

REFERENCE

800 to 1600 rpm



INVERTER-BASED RESOURCES (IBR)
Wind, solar, batteries, HVDC

ELECTRONIC:
voltage & frequency
are engineered by
computer algorithms

- 1. NEEDS VOLTAGE** reference (today)
- 2. FAST:** Changes in ~microseconds
- 3. CUSTOMIZABLE:** Extremely configurable

Steady state voltage stability: Voltage can collapse in weak grids w/ higher power injection + high IBRs

E.g. WECC Western Wind & Solar Integration Study



Regulatory note:

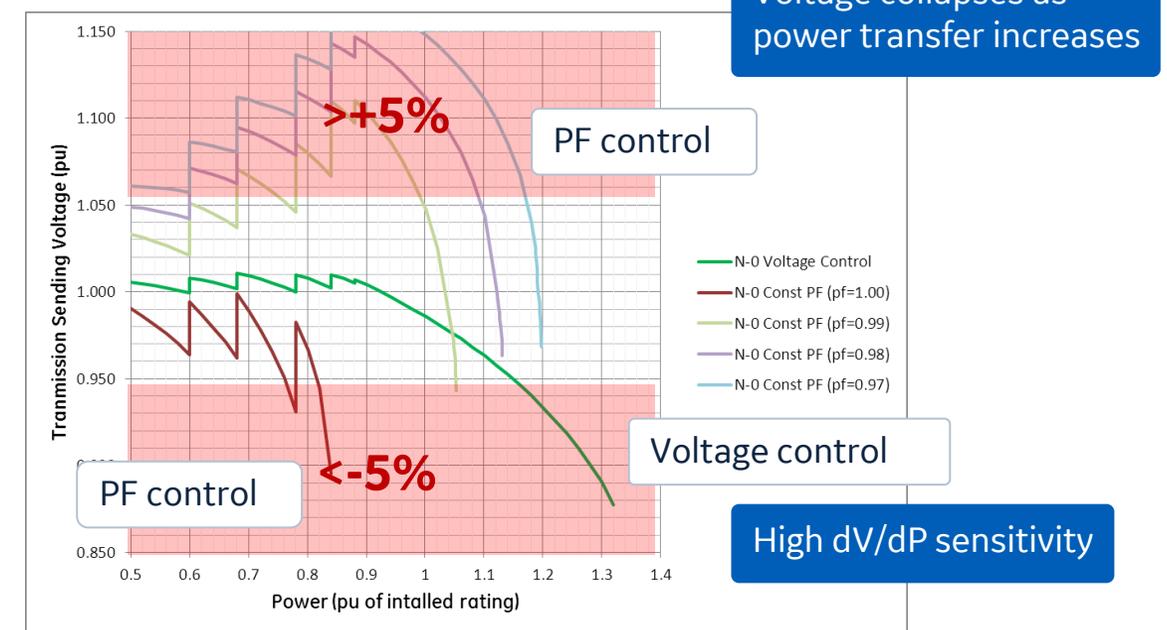
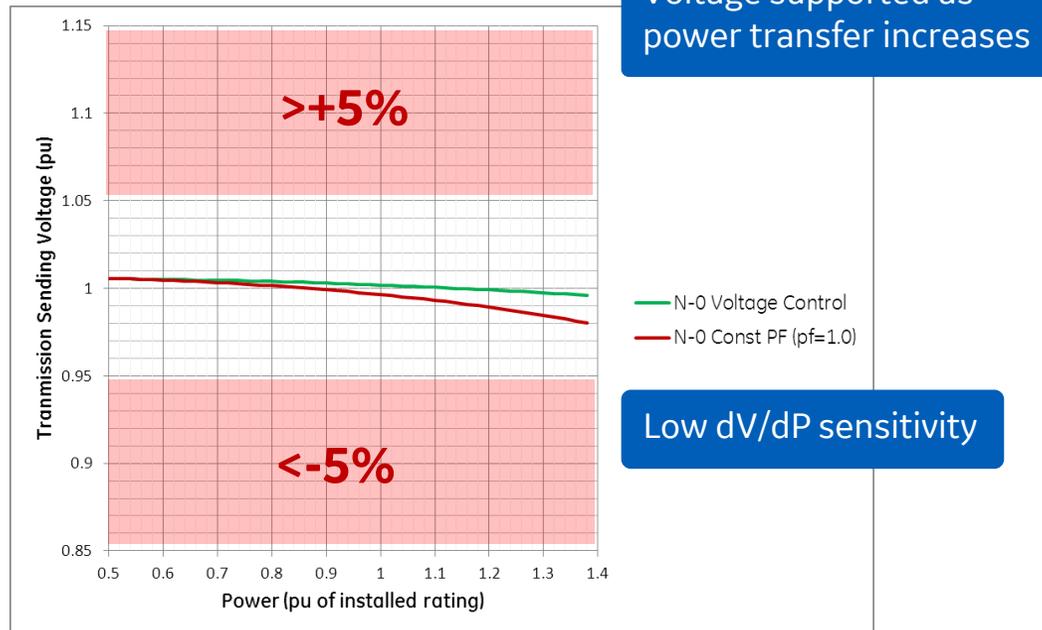
NERC VAR -002¹ closed loop voltage regulation is required.

STRONG GRID (e.g. low %IBR)

Voltage is insensitive to power injection

WEAK GRID (e.g. high %IBR)

Voltage collapses w/higher power injection

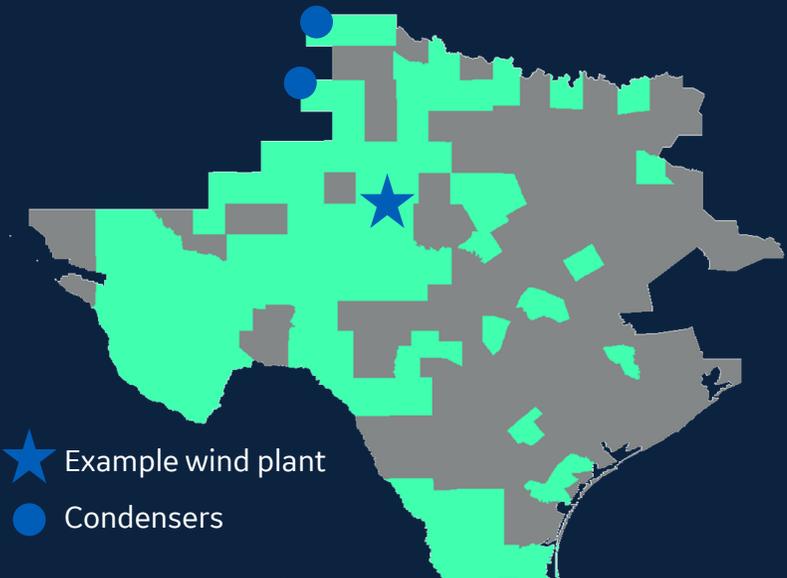


Dynamic voltage stability: voltage can collapse after a weak grid disturbance



e.g. Onshore wind plant in West Texas

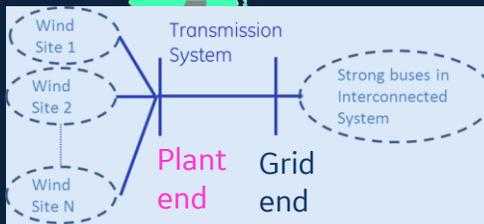
e.g. ERCOT: LOW %SM IN PANHANDLE WEAKENS VOLTAGE REFERENCE



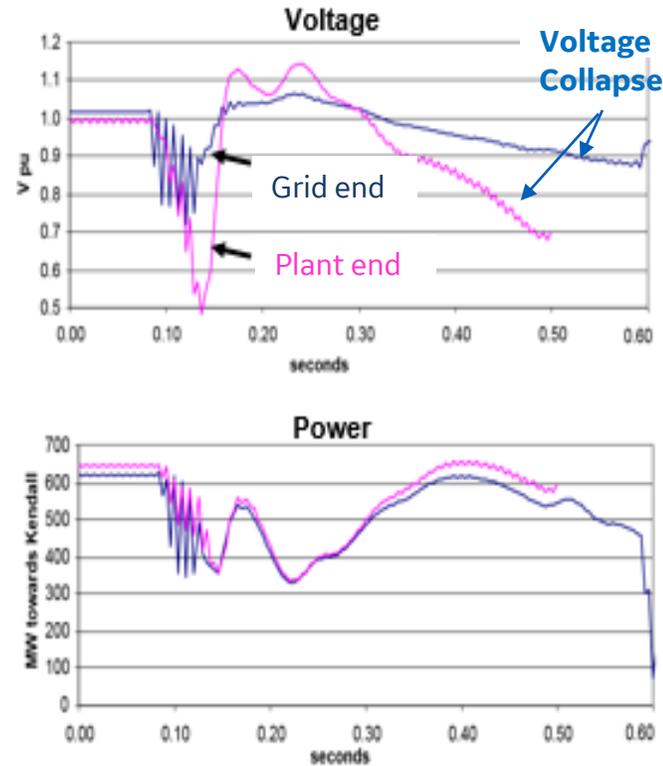
% IBR by county ('20)

- <30%
- 30-60%
- >60%

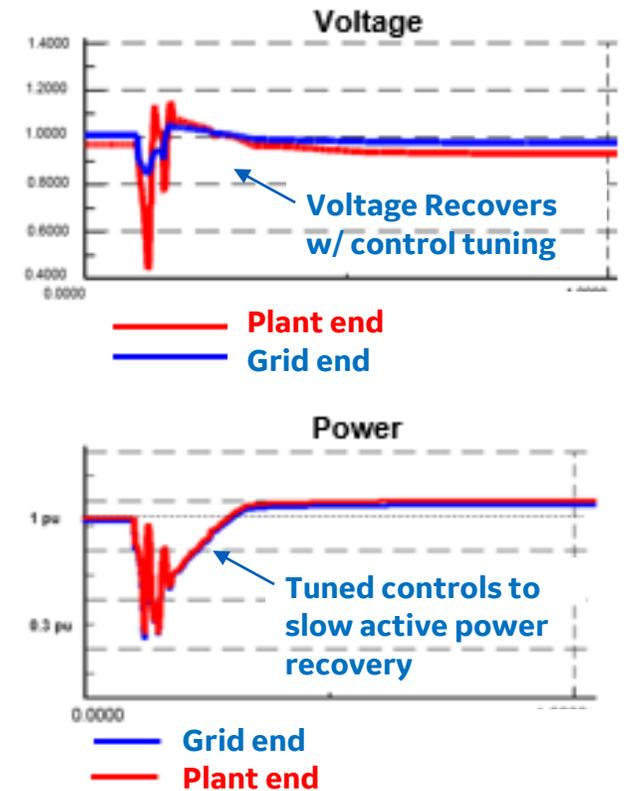
Ref: ABB, ERCOT



Field measurements: Voltage collapse due to weak grid



Simulated mitigation: Tuning controls to avoid voltage collapse



- Extremely weak application cause risk of voltage collapse
- Stable at fault clearing, collapse during power pickup before improvements
- Time frame of collapse is dictated by active power recovery

Controls stability: IBRs have multiple control layers & control modes that depend on voltage reference ... weak reference -> confusion



	RESPONSE TIME	LOAD FLOW	DYNAMICS	TRANSIENTS
LAYERS OF WIND PLANT CONTROL				
1. Turbine level	1-10 sec	Only models a static output vs. a change in output	✓	✓
2. Converter level Inner loop	200 ms		Simplified	✓
Outer loop	1 sec		✓	✓
3. Plant level	10-20 sec		✓	✓
4. Plant to plant level	10-20 sec		✓	✓
CONTROL MODES OF OPERATION				
1. Turbine level 1) Normal 2) Ride-thru torque control 3) Ride-thru energy management	200 ms	Only models a static output vs a change in output		✓
2. Converter level 1) Normal 2) Under/over freq ride-thru 3) Under/over voltage ride-thru 4) SSCI damping	200 ms			✓

Different modes ensure turbine safety

Different modes provide grid reliability services

- Turbines and converters switch control modes based on grid voltage and frequency
- In weak grids, large voltage fluctuations may lead to confusion across plants, control layers and/or control modes

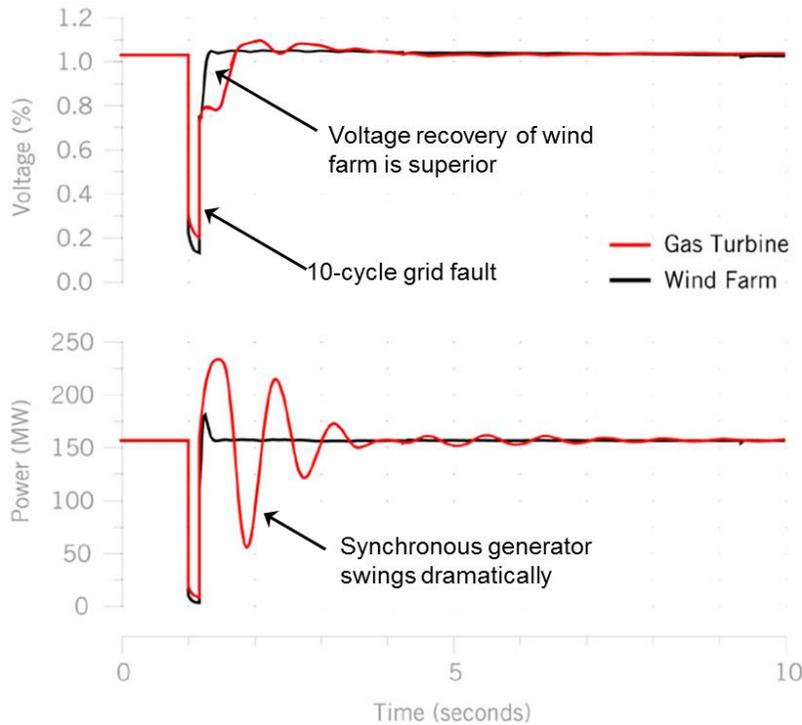
Angular stability: Weak grids can increase angular stability risk ... SMs may lose synchronism after faults



e.g. GE simulation from New York 2004

RESPONSE TO 10 CYCLE FAULT

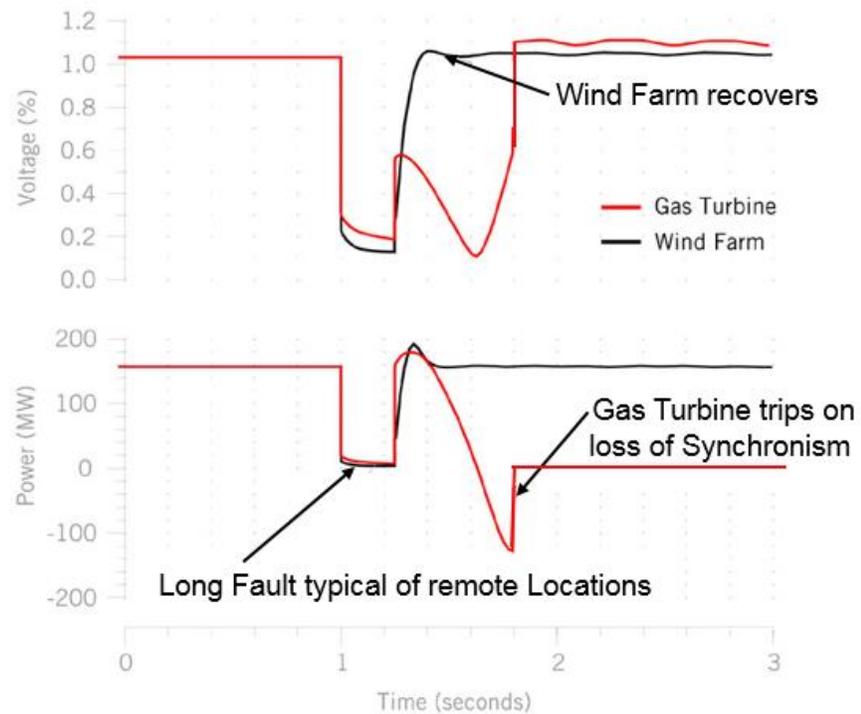
IBR & GT voltage recovers



Inverter-based resources can be more stable than conventional synchronous generators regarding transient stability, but can eventually cause a high-stress grid to fail faster and with less warning

RESPONSE TO 20 CYCLE FAULT

IBR voltage recovers but GT doesn't

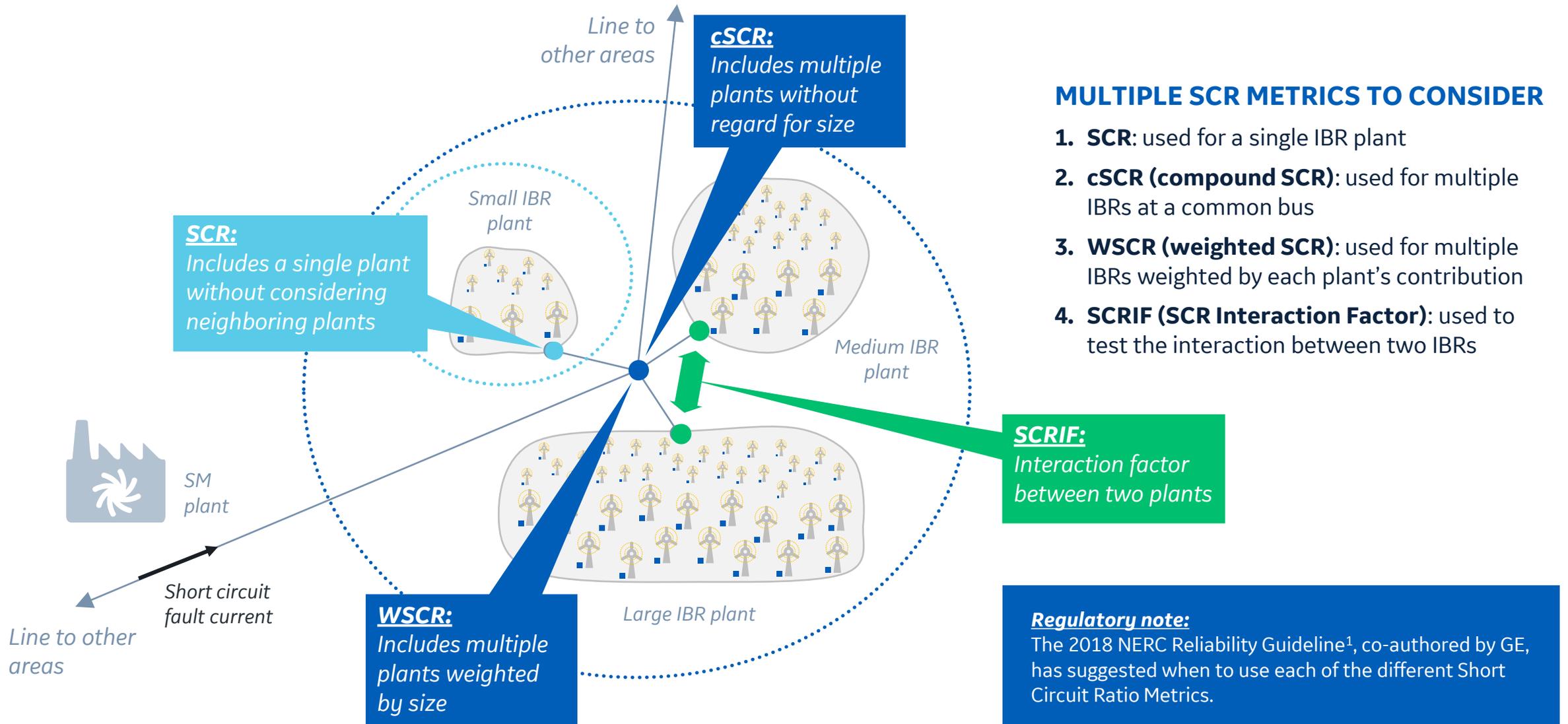


Long duration disturbances can trip conventional synchronous generators due to physical properties of the machine (critical clearing time, pole slips, loss of synchronism)

Loss of synchronism can be local or regional

Short Circuit Ratio (SCR) screening:

GE recommends using weighted SCR in NY since it accounts for plant size



1 - https://www.nerc.com/comm/RSTC_Reliability_Guidelines/Inverter-Based_Resource_Performance_Guideline.pdf
NYISO IBR ROADMAP PROJECT

Example: How to calculate SCR & WSCR?



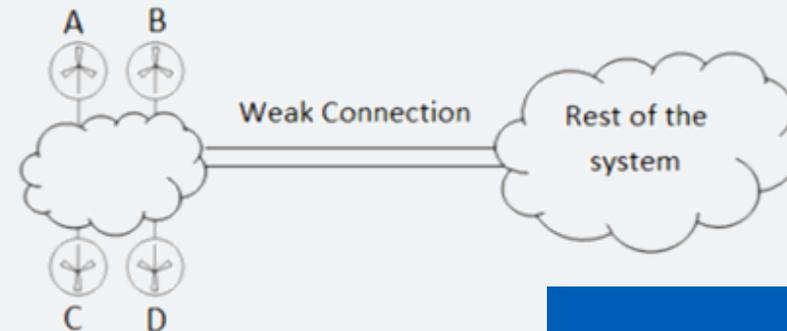
MW_{VER} **SCMVA_{POI}**

Table E.1: Wind Capacity and SCR Values Assuming No Interaction

Wind plant	Wind Capacity (MW)	Short Circuit Capacity (SCMVA)	SCR
A	1,200	6,500	5.42
B	1,000	8,000	8.00
C	800	8,500	10.63
D	2,000	7,000	3.5

SCR: FOR INDIVIDUAL PLANTS

$$SCR_{POI} = \frac{SCMVA_{POI}}{MW_{VER}}$$



WSCR: FOR GROUPINGS OF PLANTS

$$WSCR = \frac{\sum_i^N SCMVA_i * MW_{VERi}}{(\sum_i^N MW_{VERi})^2}$$

$$WSCR = \frac{1,200 * 6,500 + 1,000 * 8,000 + 800 * 8,500 + 2,000 * 7,000}{(1,200 + 1,000 + 800 + 2,000)^2} = 1.46$$

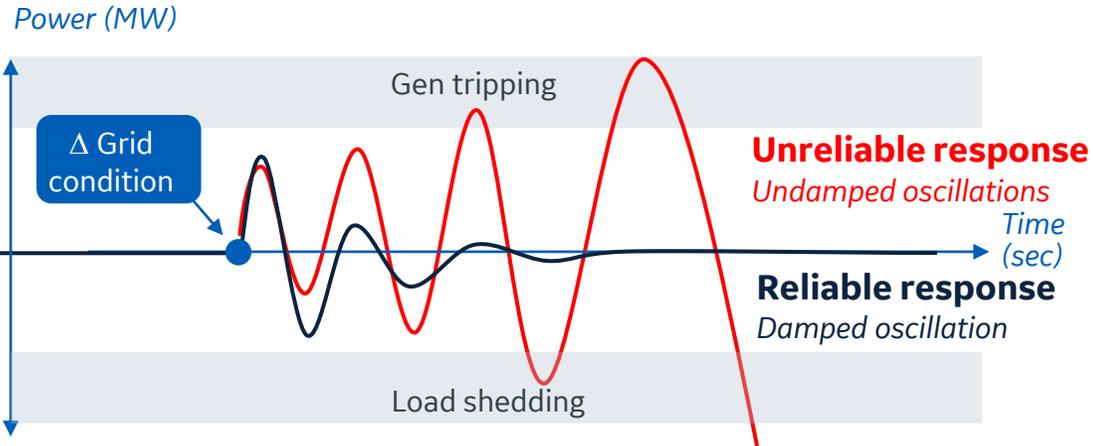
WSCR is weaker than individual SCRs due to plant-to-plant interaction

“Small signal stability”: Change in grid condition can trigger power oscillations

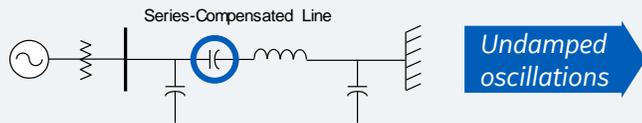
Grid operators often overlook this risk ... can result in equipment damage if undetected



Power oscillations grow in undamped systems



Ex: Sub-synchronous resonance (SSR) can break shafts



Western US: Long radial lines use series compensation to lower reactive losses

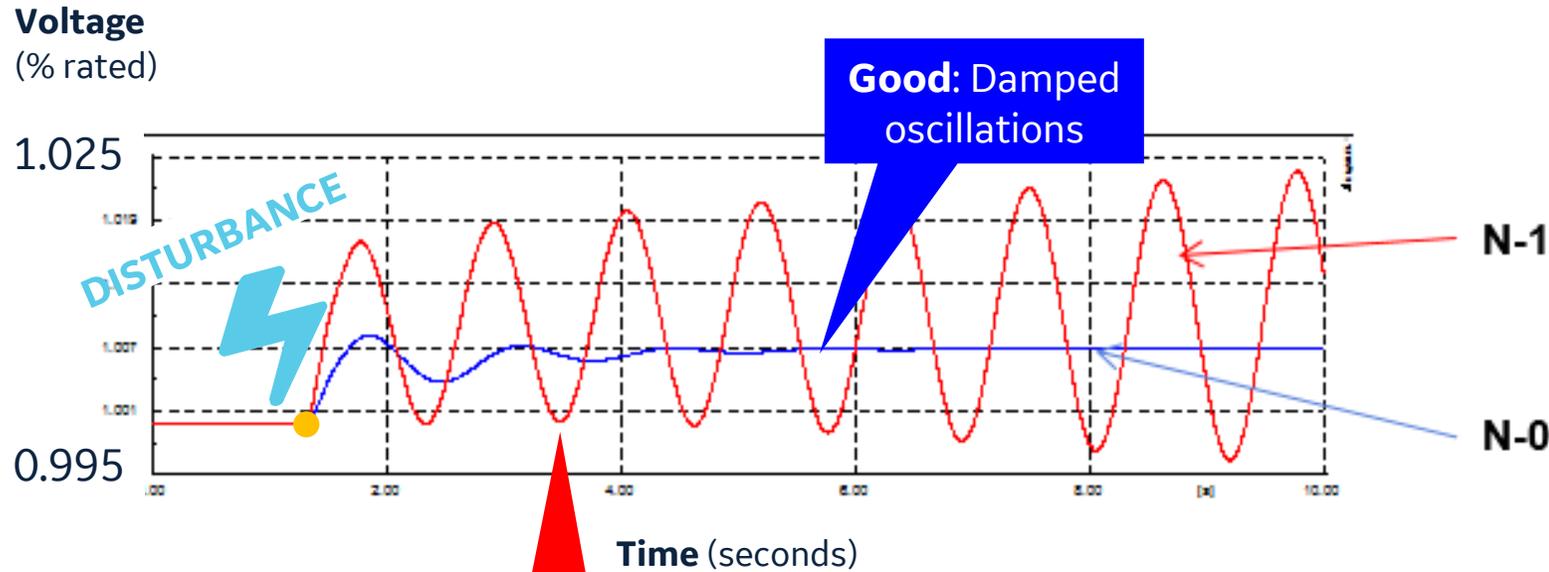
Mohave 1971: SSR breaks 1st GE generator shaft

New IBRs can trigger power oscillations ...

IN GRIDS WITH ...	RESULT	AFFECTS	FREQUENCY
IBRs w/high AC cable shunt capacitance	Shunt resonance	IBRs	~180 - 600Hz
IBRs & HVDC	Controls confusion (e.g. due to SSR, weak grids)	IBRs, SMs	~10 - 40 Hz
Series capacitors	Sub-synchronous resonance (SSR)	Synchronous machines (SM)	~ 10 - 40 Hz
High speed exciters	Local mode power oscillation	SMs	~ 3 Hz
Fast exciters/fast governor response	Inter-area power oscillation	SMs, IBRs	~1 Hz

Fast
↑
↓
Slow

Texas example: Voltage may be N-0 stable but not N-1



DISTURBANCE @t = 1s

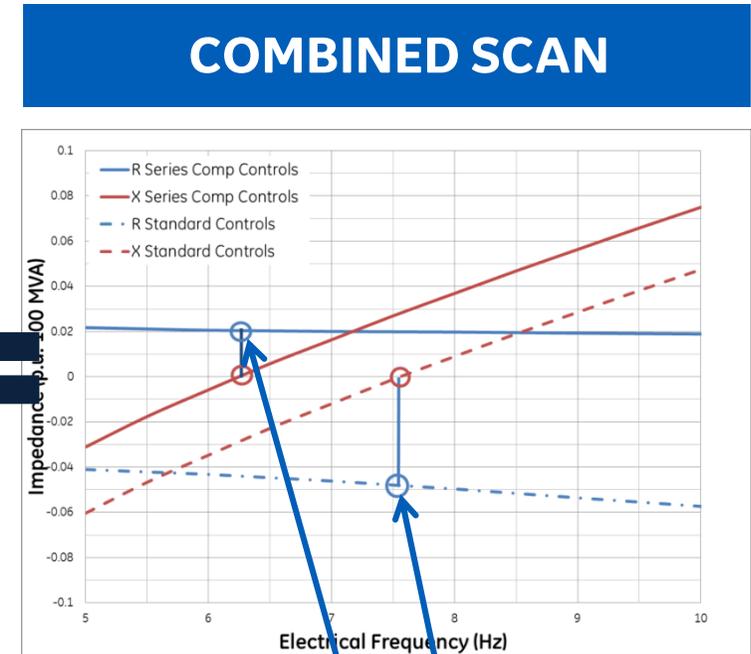
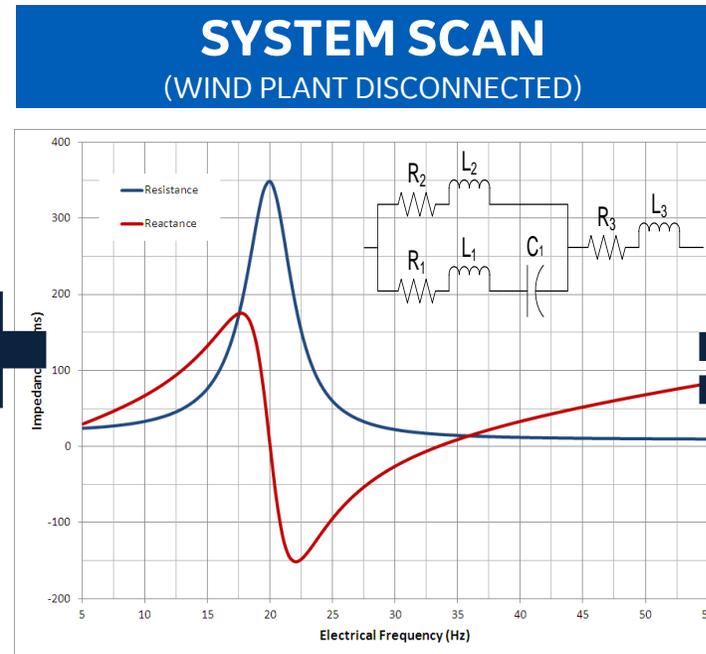
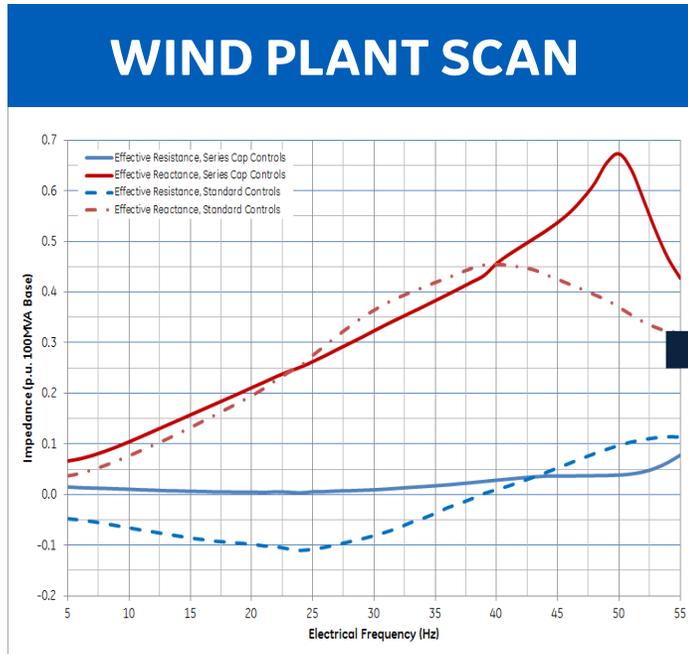
- Interaction between wind plant control layers may create **unwanted voltage oscillations**
- **N-0 grid may be strong enough** to damp out oscillations
- **N-1 grid may not be strong enough** and oscillations may grow and lead to unit tripping/blackouts

Possible upgrades:

- Control tuning
- Synchronous condensers
- Line reinforcements
- FACTS devices

Cheapest mitigation

Frequency scan to screen for small signal stability risks



- - - - - Standard controls
————— Tuned controls for small signal risk

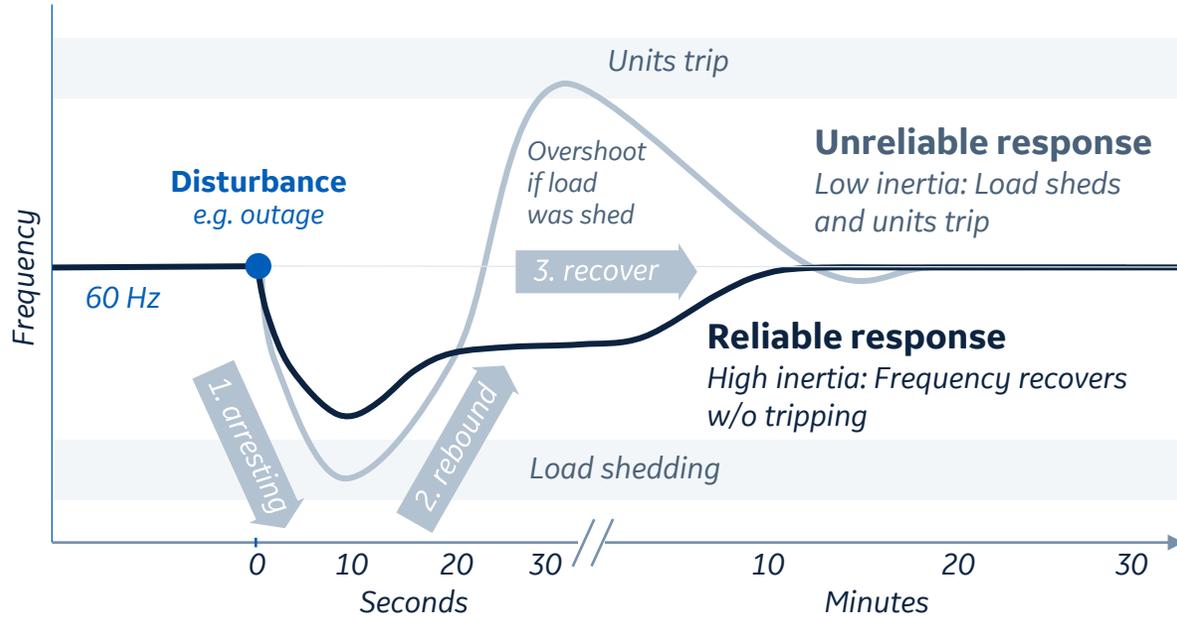
Frequency scan steps:

1. Determine equivalent impedances for wind plant & grid
2. Generate plot of total reactance and total resistance as a function of frequency.
3. Generate combined frequency scan by adding the effective resistance & reactance for the wind plant + system
4. Screen for frequencies with negative resistance. For combined frequency scan plot, frequencies at which the resistance is negative for a zero impedance correspond to unstable oscillations.

Negative resistance => **Potential unstable Resonance**

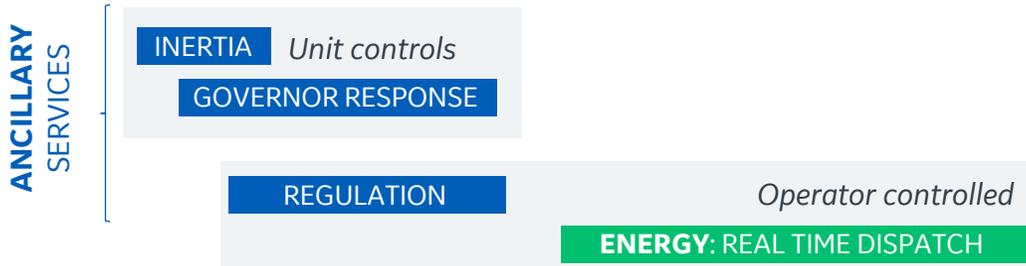
Tuned IBR controls => Positive resistance => **Positive damping & Stable oscillation**

“Frequency stability”: Grid disturbances disrupt frequency ... does a high IBR grid have appropriate frequency response to recover to 60 Hz?



HIGHER IBRs CAN MAKE FREQUENCY RESPONSE MORE “BOUNCY”

Post-disturbance period	Equipment response		Risk w/high IBRs
	SMs	IBRs	
1. Arresting (<5 sec)	Inertia High inertia w/ mechanical rotation	FFR Fast frequency response ... low inertia	Frequency drops too quickly
2. Rebound (10-20 sec)	Governor response	PFR Primary frequency response	PFR doesn't react quickly enough -> load shedding
3. Recovery (>20 sec)	Regulation		Conflict with FFR & PFR



Stable frequency response possible w/high IBRs ... **controls coordination req'd.**